Real-time model predictive control of a motion simulator based on cable robot technology

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MPI CableRobot Motion Simulator



Video

Sensors and Actuators



- Actuators
 - 8 winches controlled by motor current
- Direct sensors
 - 8 cable tension sensors located in pulley axes
 - 8 motor position sensors (encoders)
 - I IMU on the platform

OCP formulation: dynamics of the motion system

- Rigid body dynamics with 8 cable forces and gravity force.
- Additional external force and torge as a disturbance.
- Assume that the cable forces are directly controlled.
- Cables mass, cables elasticity, pulleys and winches dynamics, friction forces are not modelled.
- System state is described by the position of center of mass r, orientation quaternion q, velocity of center of mass v and rotational velocity ω:

$$\mathbf{x} = \begin{bmatrix} \mathbf{r} \\ \mathbf{q} \\ \mathbf{v} \\ \omega \end{bmatrix}$$

System dynamics: ODE

$$\dot{\mathbf{r}} = \mathbf{v}$$

$$\dot{\mathbf{v}} = \mathbf{g} + \frac{1}{m} \left(\sum_{i} \mathbf{F}_{i} + \mathbf{F}_{ext} \right)$$

$$\dot{\omega} = I^{-1} \left(\sum_{i} \mathbf{b}_{i} \times \left(R(\mathbf{q})^{\top} \mathbf{F}_{i} \right) + \tau_{ext} - \omega \times \left(I \omega \right) \right)$$

$$\dot{\mathbf{q}} = \frac{G(\mathbf{q})^{\top}}{2} \omega$$

$$\mathbf{F}_{i} = \frac{\mathbf{l}_{i}}{\|\mathbf{l}_{i}\|} f_{i}$$

$$\mathbf{l}_{i} = \mathbf{a}_{i} - \mathbf{r} - R(\mathbf{q}) \mathbf{b}_{i}$$
(1)

$$G(\mathbf{q}) = \begin{bmatrix} -q_1 & q_0 & q_3 & -q_2 \\ -q_2 & -q_3 & q_0 & q_1 \\ -q_3 & q_2 & -q_1 & q_0 \end{bmatrix}$$

- R(q) rotation matrix from platform to world frame
- ▶ *I* inertia tensor, *m* mass
- l_i vector connecting ends of *i*-th cable
- b_i, a_i coordinates of anchor point and outlet point of *i*-th cable
- f_i tension force of *i*-th cable
- $\blacktriangleright~{\bf F}_{\rm ext}$ external force
- $\tau_{\rm ext}$ external torque.



$$\mathbf{r}_{\min} \leq \mathbf{r} \leq \mathbf{r}_{\max}$$

- Linear velocity limit
- Rotational velocity limit

 $\|\omega\| \le \omega_{\max}$

 $\|\mathbf{v}\| \leq v_{\max}$

► Cable force limits

 $0 < f_{\min} \le f_i \le f_{\max}$

Unit norm of quaternion (consistency constraint)

$$\|\mathbf{q}\| = 1$$



▶ For safety and stability reasons, the platform is required to stop at the end of the horizon:

 $\mathbf{v}(T) = 0$ $\omega(T) = 0$



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Possible additional constraint: upright platform position at the end of the horizon:

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} R \left(\mathbf{q} \left(T \right) \right)^{\top} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = 0$$

OCP formulation: objective function



► The objective function

$$\min_{\mathbf{x},\mathbf{u}} \quad \sum_{k=0}^{N-1} \left(\|\mathbf{u}_{k} - \hat{\mathbf{u}}_{k}\|_{W_{\mathbf{u}}}^{2} + \|\mathbf{x}_{k} - \hat{\mathbf{x}}_{k}\|_{W_{\mathbf{x}}}^{2} + \|\mathbf{y}(\mathbf{x}_{k},\mathbf{u}_{k}) - \hat{\mathbf{y}}_{k}\|_{W_{\mathbf{y}}}^{2} \right) + \|\mathbf{x}_{N} - \hat{\mathbf{x}}_{N}\|_{W_{\mathbf{x}_{N}}}^{2}$$

s.t.

$$\mathbf{x}_{k+1} = F(\mathbf{x}_k, \mathbf{u}_k) \ \forall k = 0 \dots N - 1$$

based on (1) and assuming $\mathbf{F}_{ext} = 0, \ \tau_{ext} = 0$
and the path and terminal constraints above

where \mathbf{x} - system state, $\mathbf{u} = [f_1, f_2, \dots, f_{N_C}]^\top$ - system input, $\mathbf{y}(\cdot, \cdot)$ - output function, $\hat{\mathbf{u}}, \hat{\mathbf{x}}$ and $\hat{\mathbf{y}}$ - reference input, state and output, respectively.

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$$\begin{aligned} \mathbf{x}_{k+1} &= F(\mathbf{x}_k, \mathbf{u}_k) \; \forall k = 0 \dots N-1 \\ \text{based on (1) and assuming } \mathbf{F}_{\text{ext}} = 0, \; \tau_{\text{ext}} = 0 \\ \text{and the path and terminal constraints above} \end{aligned}$$

where \mathbf{x} - system state, $\mathbf{u} = [f_1, f_2, \dots, f_{N_C}]^\top$ - system input, $\mathbf{y}(\cdot, \cdot)$ - output function, $\hat{\mathbf{u}}, \hat{\mathbf{x}}$ and $\hat{\mathbf{y}}$ - reference input, state and output, respectively.

- The blue term is the one relevant for motion simulation.
- Choosing weights W_u, W_x and W_y allows to balance between input tracking, state tracking and output tracking.

OCP formulation: output function



In motion simulation, we want to reproduce specific force f_H , rotational velocity ω_H and rotational acceleration α_H in the reference frame attached to subject's head:

$$\mathbf{y}(\mathbf{u}, \mathbf{x}) = \begin{bmatrix} \mathbf{f}_H \\ \omega_H \\ \alpha_H \end{bmatrix}$$
$$\mathbf{f}_H = R_P^H \left(R(\mathbf{q})^\top (\mathbf{g} - \dot{\mathbf{v}}) - \underbrace{\dot{\omega} \times \mathbf{r}_H}_{\text{Euler acceleration}} - \underbrace{\omega \times (\omega \times \mathbf{r}_H)}_{\text{centrifugal acceleration}} \right)$$
$$\omega_H = R_P^H \omega$$
$$\alpha_H = R_P^H \dot{\omega}$$

where \mathbf{r}_H – position of the head in platform frame, R_P^H – rotation matrix from head frame to platform frame.

▶ Notice that the output directly depends on input ("direct feedthrough"), because of $\dot{\mathbf{v}}$ and $\dot{\omega}$ (look at (1)).



Table: MPC controller properties

HW sampling time	$pprox 1{ m ms}$
Control sampling time	50 ms
Prediction horizon (steps) N	40
Number of states	13
Number of controls	8
Integrator	Explicit RK4
Hessian approximation	Gauss-Newton
QP solver	qpOASES+condensing; HPMPC
Problem-specific code	Generated by CasADi
Implementation language	C++

Software implementation





- Based on tmpc: Templates for Model Predictive Control http://gitlab.syscop.de/ mikhail.katliar/tmpc
- ► Unified interface to QP solvers, integrators etc. ⇒ different controller implementations which use different components can be easily created.

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Table: MPC controller performance evaluation

CPU type	AMD A8-4500M @1.9 GHz
Preparation phase time	1.9 ms
Feedback phase time with qpOASES+condensing (avg.)	820 ms
Feedback phase time with HPMPC (avg.)	8.5 ms

- ▶ The controller can run at almost 100 Hz on my laptop
- > 20 Hz is the required minimum for motion simulation



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- ► The controller can run at almost 100 Hz on my laptop
- > 20 Hz is the required minimum for motion simulation
- HPMPC has made it possible (thanks Gianluca)!

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Due to direct feedthrough, for a piecewise-continuous input the output is also only piecewise-continuous:



- ► The output changes significantly by the end of a sampling interval, but only the output value at the beginning enters the objective function ⇒ poor output tracking.
- Possible remedies:
 - 1. Make input continuous by controlling cable forces change rate rather than cable forces themselves (IMPLEMENTED).
 - 2. Accurately integrate output error instead of evaluating it at one point per interval (WORTH IMPLEMENTING?).



Now time for a demo!



Thank you very much for your attention!