



Control implementations on the HIGHWIND carousel

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HIGHWIND Scientific Advisory Board (SAB) Meeting
Department of Microsystems Engineering - IMTEK
University of Freiburg, Germany

Agenda: Treating in this talk

- System identification of the carousel

- Model
- Parameter estimation

- State estimator simulations and implementation

- Discrete Linear Quadratic Estimator (DLQE)
- Disturbance state augmented DLQE (steady state Kalman Filter)

- Control simulations and implementation

- Discrete Linear Quadratic Regulator (DLQR)
- Disturbance state augmented DLQR
- Discrete Linear Quadratic Gaussian Control (DLQG)

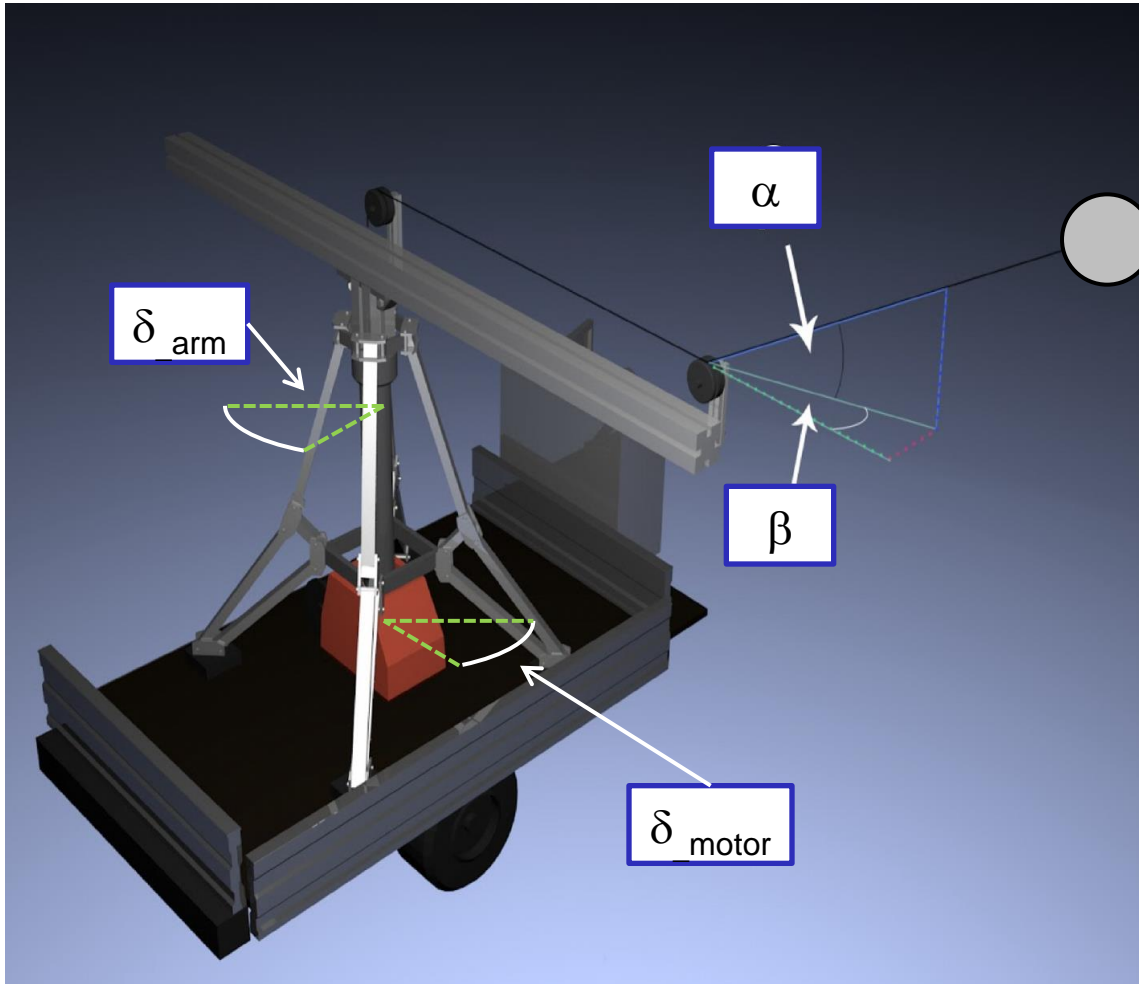
Remarks on this talk

Colors used:

- Real sensor measurements
- Numerical simulations
- References or setpoints
- Estimate simulations (DLQE, augmented DLQE, DLQG)
- Real estimator output (Implemented estimators)
- Experimental control signal (DLQR, augmented DLQR, DLQG)

For angle measurement, radians are preferred to degrees

1.0 System identification of the carousel: Actual model



Actual model considers:

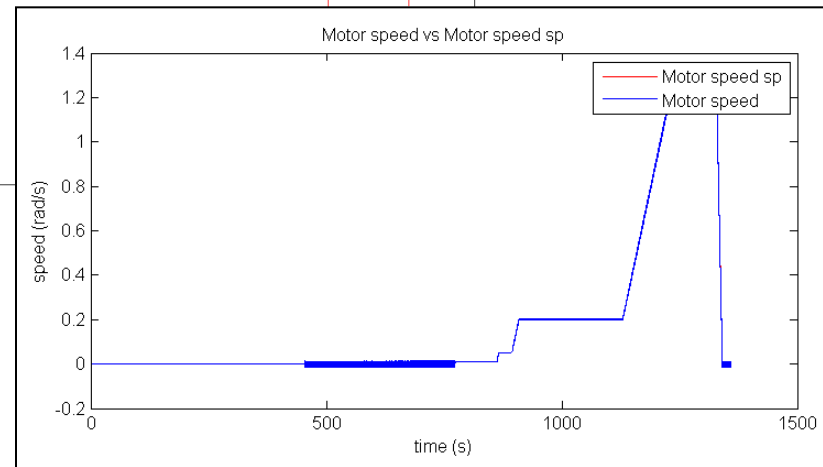
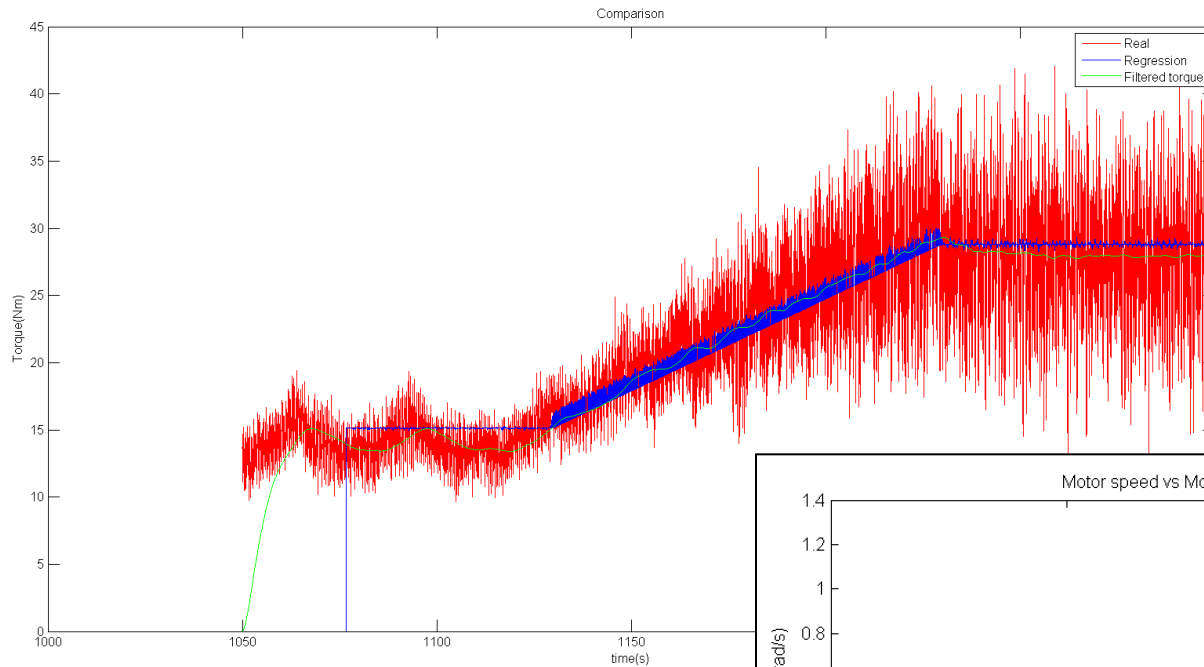
- Kinetic energy:
 - Arm inertia
 - Ball velocity
 - LAS inertia
 - LAS Attachment inertia (tether+ball)
- Potential energy
 - Ball
- Generalized torques
 - Air friction
 - LAS α friction
 - LAS β friction

1.1 Entirely physical model

Good torque prediction

$$T = I\alpha + c\omega_{motor}$$

δ_{motor}
 δ_{arm}
 α
 β
 $\dot{\delta}_{motor}$
 $\dot{\delta}_{arm}$
 $\dot{\alpha}$
 $\dot{\beta}$



Isq_inertia_friction_filter()

12/06/2015

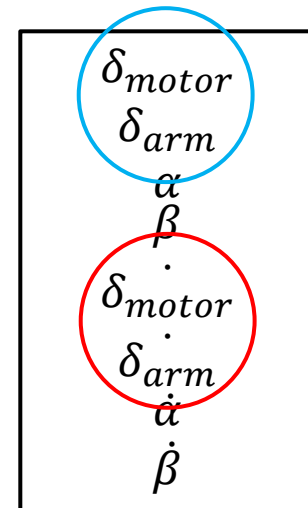
1.2 Physical model detailed

Advantages:

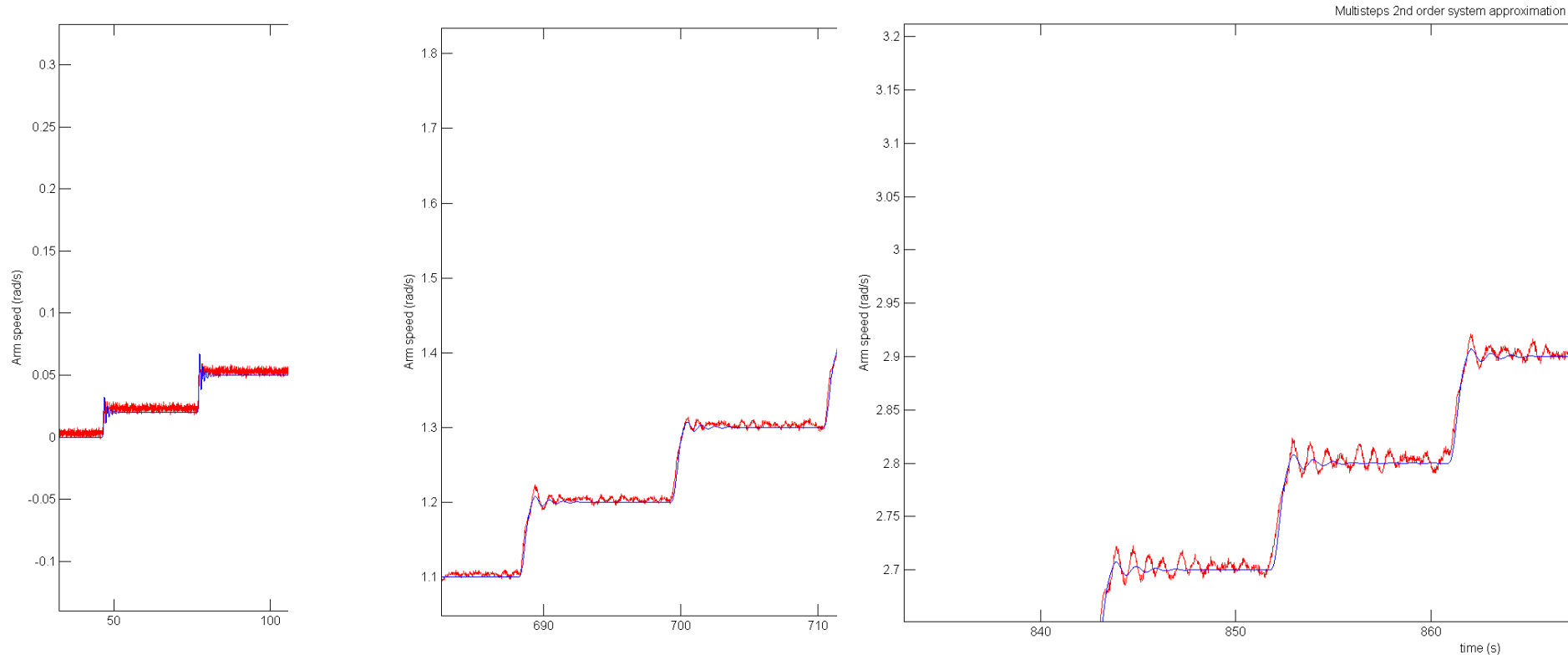
- Differentiate between motor and arm state
- Six first states already being measured and reported

Disadvantages

- Coupling between motor speed and arm speed difficult to measure (rubber band)
- Input: Motor speed setpoint. Motor speed already modified by lower level controllers, algorithm difficult to estimate



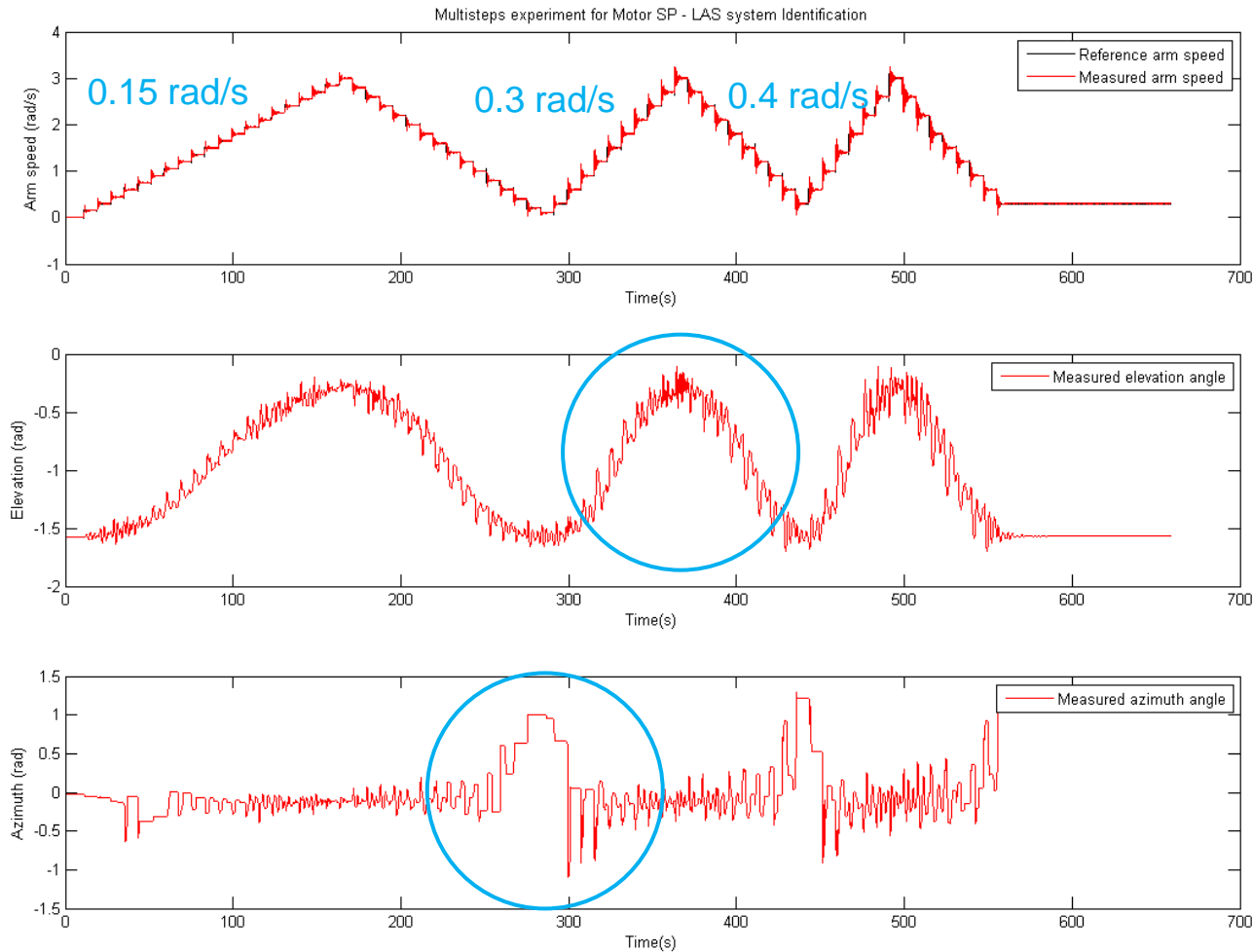
2.1 Idea: $\dot{\delta}_{\text{motor_sp}} \rightarrow \dot{\delta}_{\text{arm}}$ as second order system



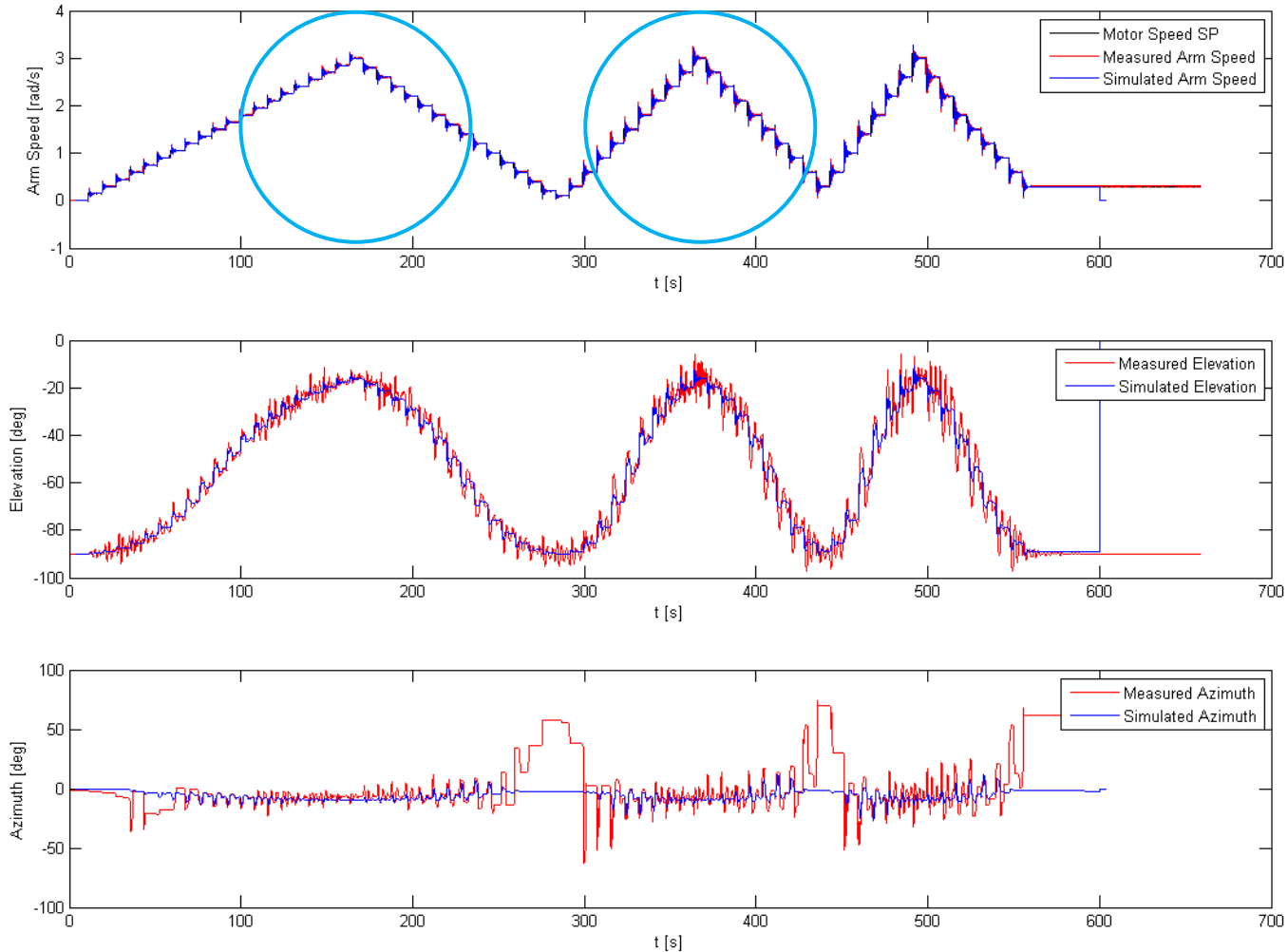
----- Real arm speed - - - - Simulated arm speed

3.1 LAS Identification

Multi-steps experiment (avoidance of low speeds)

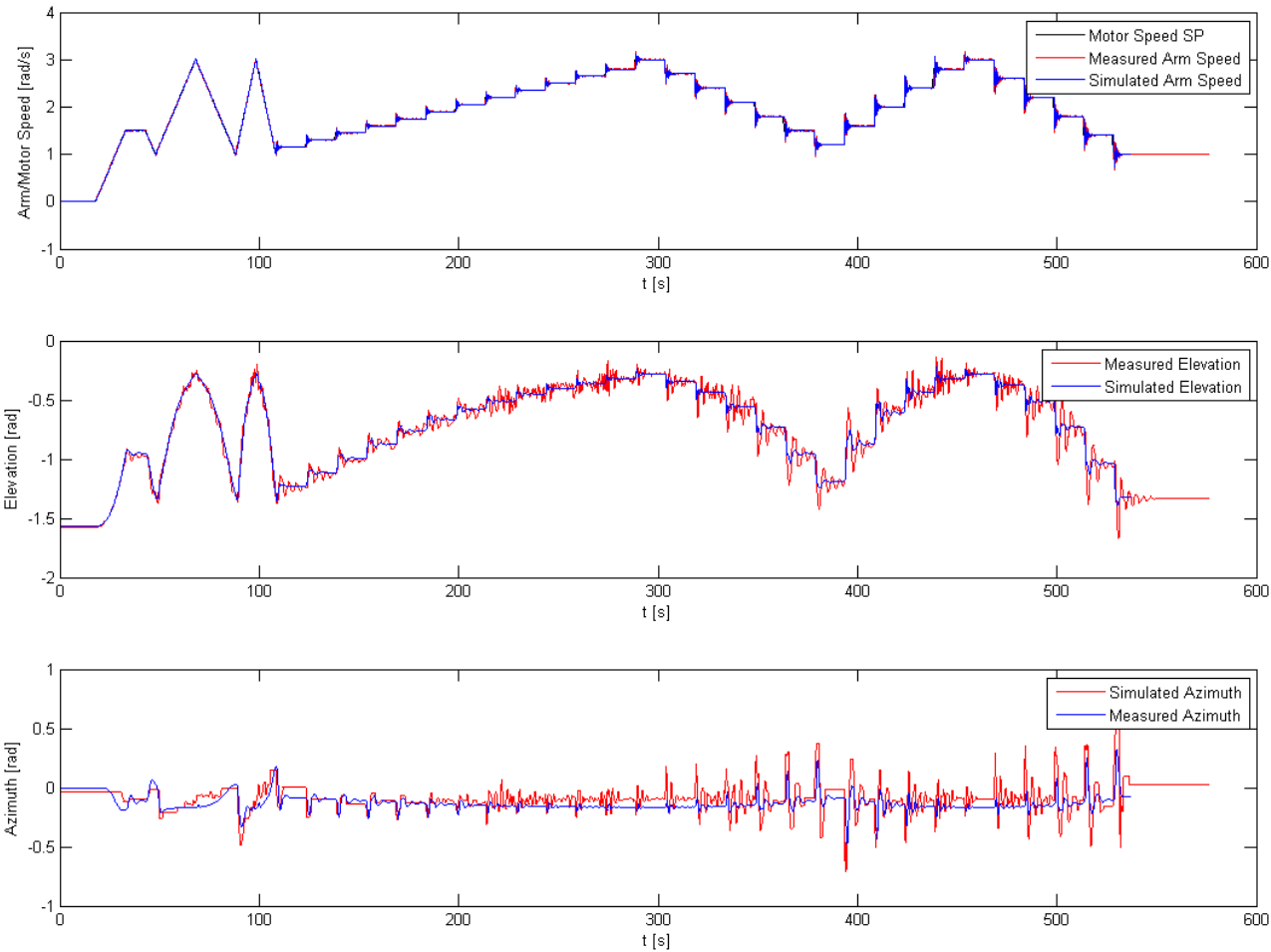


3.2 LAS Identification - Simulation



siemens_step_response_experiment ()

3.3 LAS Identification – Acceptable working range

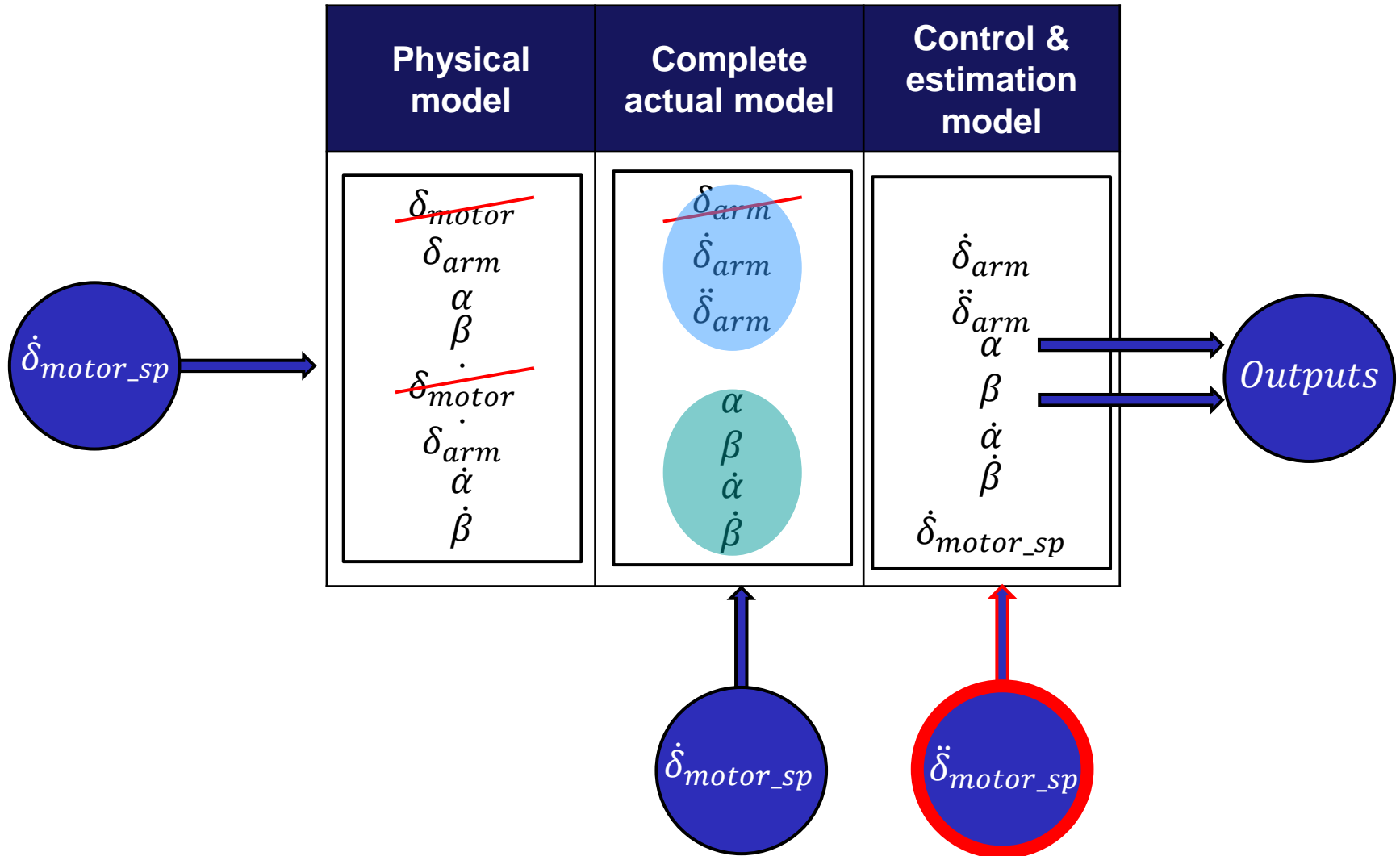


final_step_response_experiment ()

3.4 LAS model parameters

Description	Symbol	Conf. Int.	Covariance matrix																
Air-Ball friction	μ_{air}	0.0069 kg/m	<div style="border: 1px solid black; padding: 10px; text-align: center;"> <p>1.0e-03 *</p> <table style="margin: auto;"> <tr> <td>0.000002</td> <td>-0.000002</td> <td>-0.000011</td> <td>-0.000006</td> </tr> <tr> <td>-0.000002</td> <td>0.062871</td> <td>0.009529</td> <td>-0.009383</td> </tr> <tr> <td>-0.000011</td> <td>0.009529</td> <td>0.176314</td> <td>-0.007819</td> </tr> <tr> <td>-0.000006</td> <td>-0.009383</td> <td>-0.007819</td> <td>0.007186</td> </tr> </table> </div>	0.000002	-0.000002	-0.000011	-0.000006	-0.000002	0.062871	0.009529	-0.009383	-0.000011	0.009529	0.176314	-0.007819	-0.000006	-0.009383	-0.007819	0.007186
0.000002	-0.000002	-0.000011		-0.000006															
-0.000002	0.062871	0.009529		-0.009383															
-0.000011	0.009529	0.176314		-0.007819															
-0.000006	-0.009383	-0.007819	0.007186																
Elevation LAS friction	$\mu_{\alpha,LAS}$	1.4351 Nms/rad																	
Azimuth LAS friction	$\mu_{\beta,LAS}$	0.6122 Nms/rad																	
Constant attached inertia	$I_{attached_LAS}$	0.2853 kg/m ²																	

3.5 Model adaptation



4.1 Discrete Linear Quadratic Estimator (DLQE) design

$$\min_{x_0 \dots x_k} \left\| x_0 - \hat{x}_0 \right\|_{P_0}^2 + \left\| x_k - \hat{x}_k \right\|_W^2 + \left\| y_k - \hat{y}_k \right\|_V^2$$

$$x_{k+1} = Ax_k + Bu_k + Gw_k$$

$$s.t. \quad y_k = Cx_k + Du_k + v_k$$

- Linearization at $x_{SS} = [1.5878 \quad -0.8802 \quad -0.0687 \quad 0 \quad 0 \quad 0 \quad 1.5878]$
- Discretization with $\Delta_t = 100ms$ and initial estimate $\bar{x}_0 = x_{SS}$

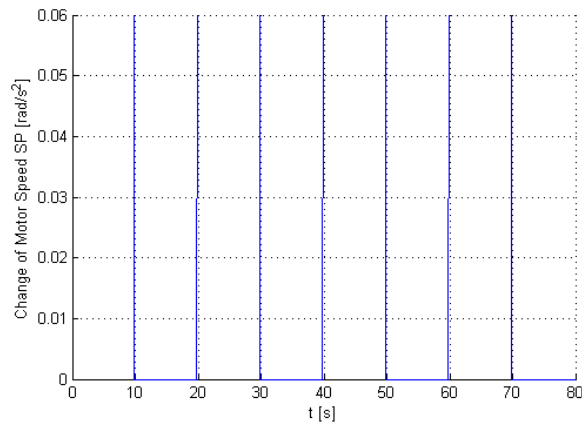
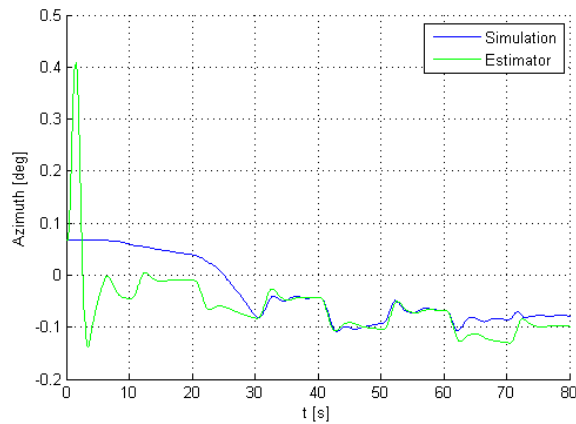
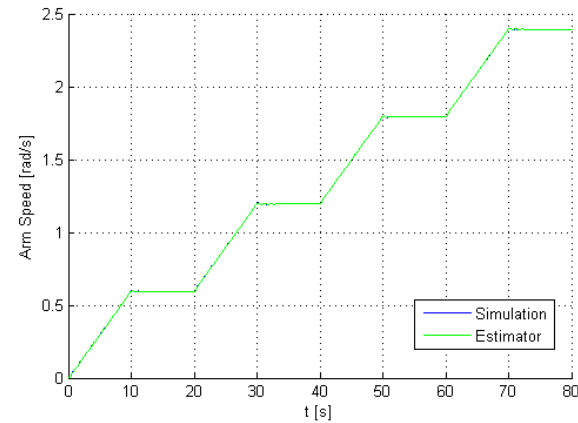
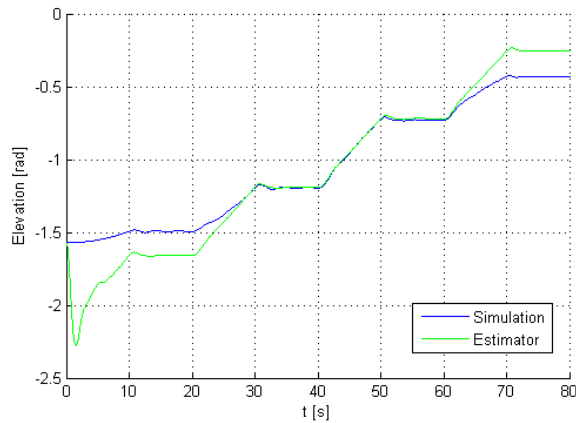
$$x = \begin{bmatrix} \dot{\delta}_{arm} \\ \ddot{\delta}_{arm} \\ \alpha \\ \beta \\ \dot{\alpha} \\ \dot{\beta} \\ \dot{\delta}_{motor_sp} \end{bmatrix} \quad Q_E = \begin{bmatrix} w_n^2 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & w_n^2 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & w_o^2 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & w_o^2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & w_n^2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & w_n^2 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad R_E = \begin{bmatrix} v_n^2 & 0 \\ 0 & v_n^2 \end{bmatrix} \quad G = I_{n_x \times n_x}$$

$$v = 0.01$$

$$w_n = 0.001$$

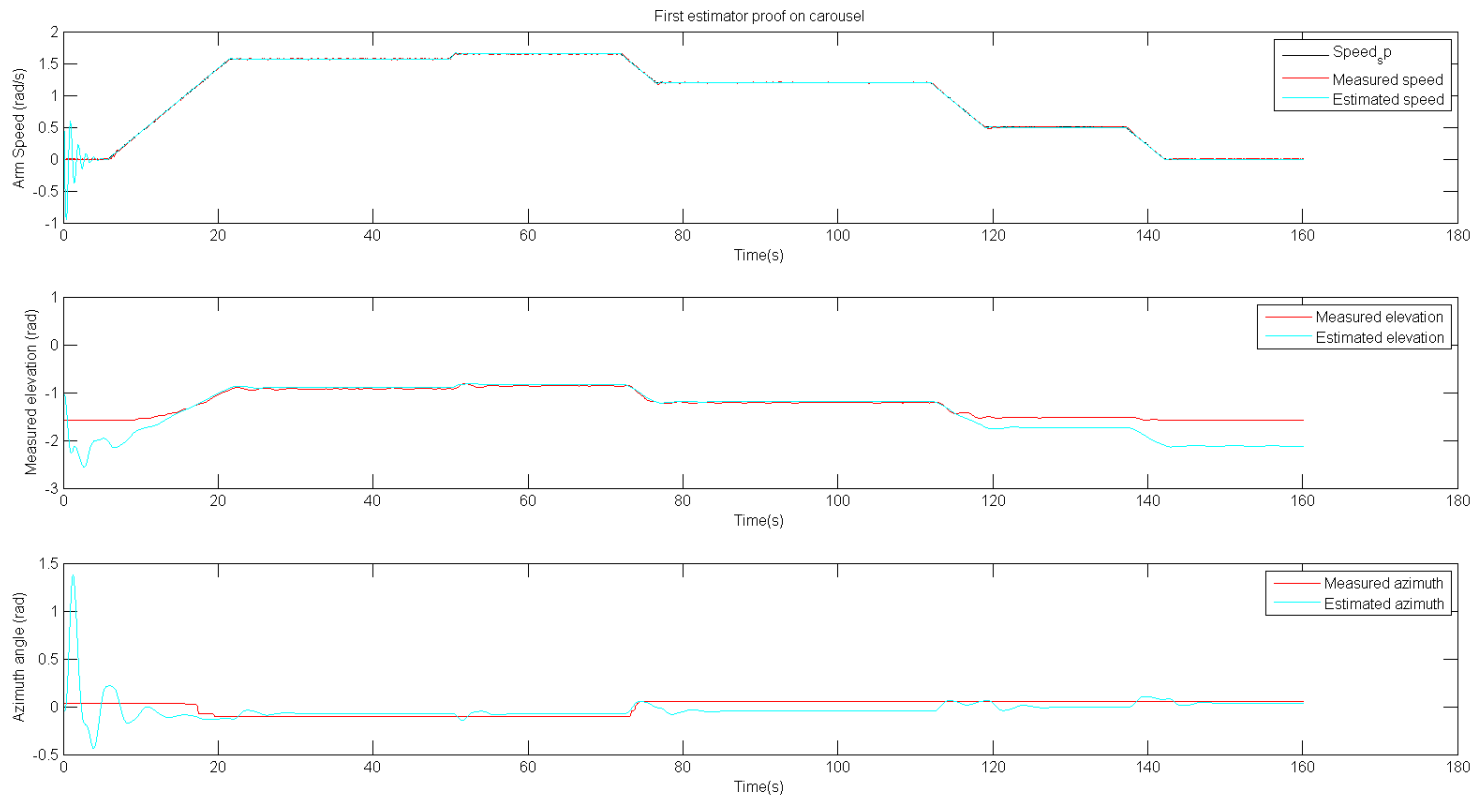
$$w_o = 1 \times 10^{-6}$$

4.2 DLQE Simulation



estimator_simulation()

4.3 DLQE: Experimental Results



`kalman1()`

4.4 Disturbance state augmented DLQE design

Staying at the linearization setpoint is unlikely for such a setup (tether length varied constantly)

- Mismodelling in elevation angle corrected by the use of an added disturbance state

$$\alpha = \ddot{\alpha} + S_p$$
$$\dot{S}_p = -\frac{S_p}{\tau} + w_{n_s} \text{ with } w_{n_s} \sim N(0, \Sigma())$$

- Design characteristics: $\tau = 100$ and $w_{n_s} = 0.001$

4.5 Model changes due to augmentation

Physical model	Complete actual model	Control & estimation model	Augmented control model
δ_{motor} δ_{arm} α β $\dot{\delta}_{motor}$ $\dot{\delta}_{arm}$ $\dot{\alpha}$ $\dot{\beta}$	δ_{arm} $\dot{\delta}_{arm}$ $\ddot{\delta}_{arm}$ α β $\dot{\alpha}$ $\dot{\beta}$	$\dot{\delta}_{arm}$ $\ddot{\delta}_{arm}$ α β $\dot{\alpha}$ $\dot{\beta}$ $\dot{\delta}_{motor_sp}$	$\dot{\delta}_{arm}$ $\ddot{\delta}_{arm}$ α β $\dot{\alpha}$ $\dot{\beta}$ $\dot{\delta}_{motor_sp}$ S_p

4.6 Augmented DLQE: initial tuning

- Linearization at $x_{SS} = [1.6196 \quad -0.8802 \quad -0.0696 \quad 0 \quad 0 \quad 0 \quad 1.6196]$
- Discretization with $\Delta_t = 20ms$ and initial estimate $\bar{x}_0 = x_{SS}$

$$x = \begin{bmatrix} \delta_{arm} \\ \ddot{\delta}_{arm} \\ \alpha \\ \beta \\ \dot{\alpha} \\ \dot{\beta} \\ \delta_{motor_sp} \\ s_p \end{bmatrix} \quad Q_E = \begin{bmatrix} w_n^2 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & w_n^2 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & w_o^2 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & w_o^2 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & w_n^2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & w_n^2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & w_s \end{bmatrix} \quad R_E = \begin{bmatrix} v_n & 0 \\ 0 & v_n \end{bmatrix} \quad G = I_{n_x \times n_x}$$

$$v = 0.002$$

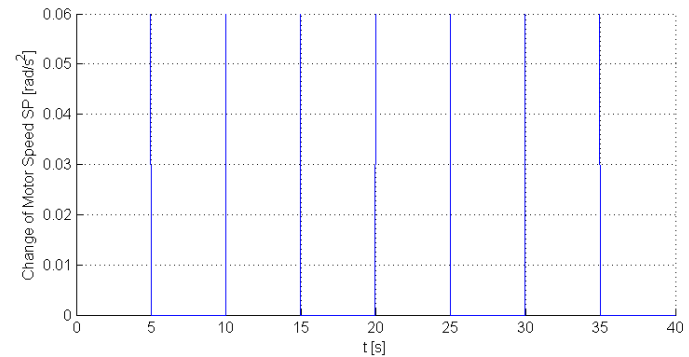
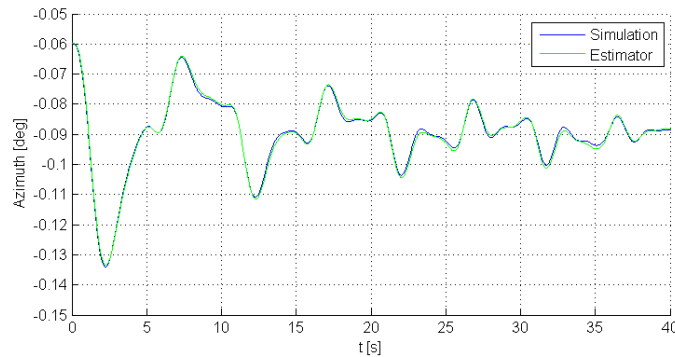
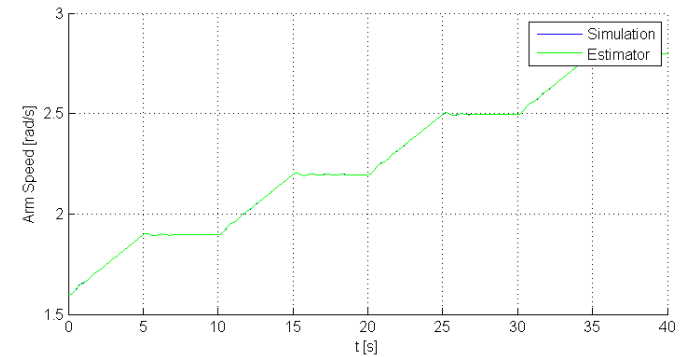
$$w_n = 0.001$$

$$w_o = 1 \times 10^{-6}$$

$$w_s = 0.01$$

4.7 DLQE Simulation

***Experiment and fine tuning to be seen during the visit**



`estimator_simulation()`

5.1 Discrete Linear Quadratic Regulator (DLQR) design

$$\min_{x_0 \dots x_N \dots u_0 \dots u_{N-1}} \|x_N\|_{P_N}^2 + \|x_k\|_Q^2 + \|u_k\|_R^2$$

$$x_{k+1} = Ax_k + Bu_k$$

$$s.t. \quad x_o - \bar{x}_o = 0$$

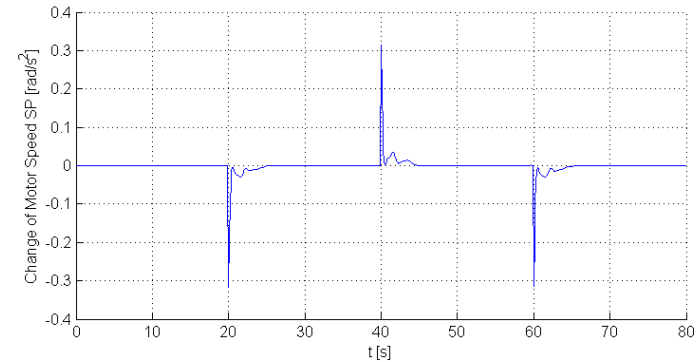
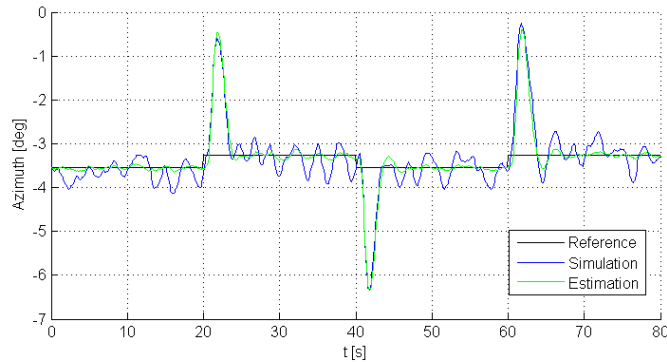
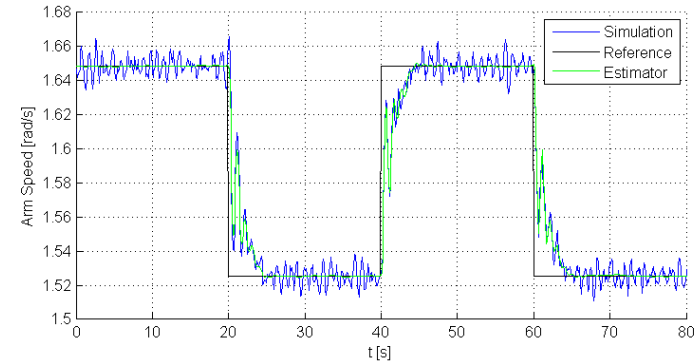
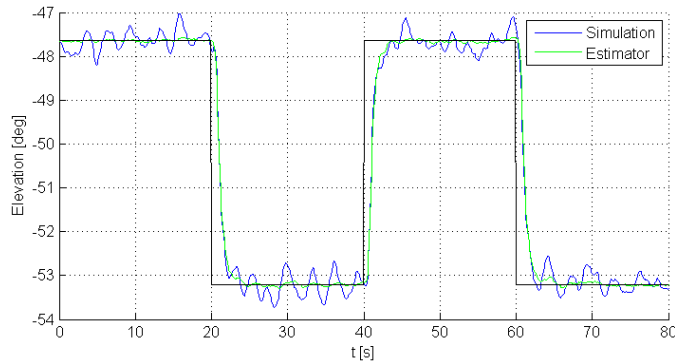
- Linearization at $x_{ss} = [1.5878 \quad -0.8802 \quad -0.0687 \quad 0 \quad 0 \quad 0 \quad 1.5878]$
- Discretization with $\Delta_t = 100ms$ and initial estimate $\bar{x}_0 = x_{ss}$

$$x = \begin{bmatrix} \dot{\delta}_{arm} \\ \ddot{\delta}_{arm} \\ \alpha \\ \beta \\ \dot{\alpha} \\ \dot{\beta} \\ \dot{\delta}_{motor_sp} \end{bmatrix} \quad Q = \begin{bmatrix} q_0^2 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & q_0^2 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 8^2 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & q_0^2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 5^2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & q_0^2 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & q_0 \end{bmatrix} \quad R = [2^2]$$

$$P_N = [0]$$

$$q_0 = 1 \times 10^{-6}$$

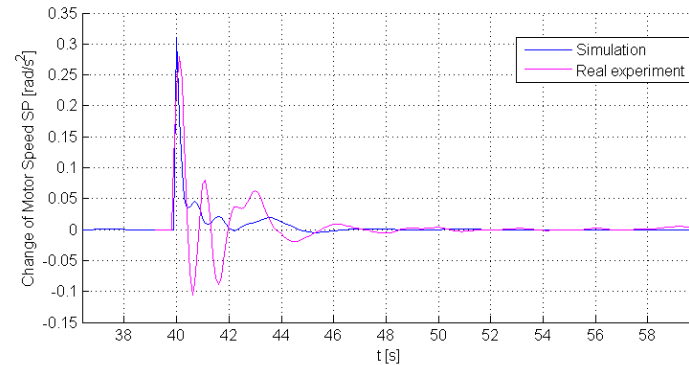
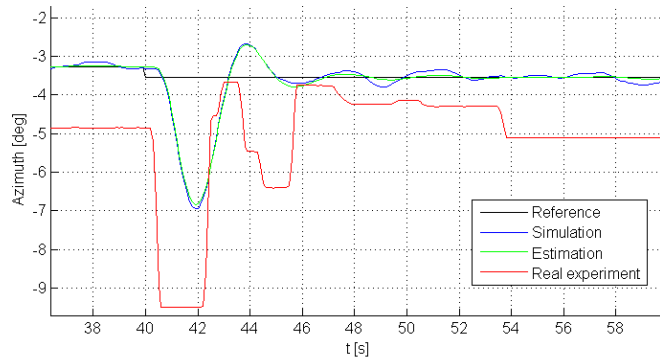
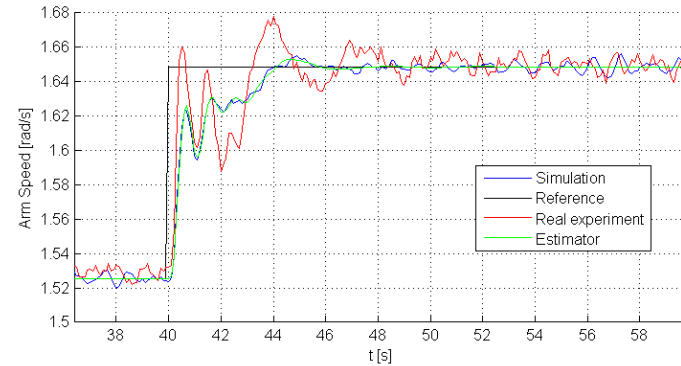
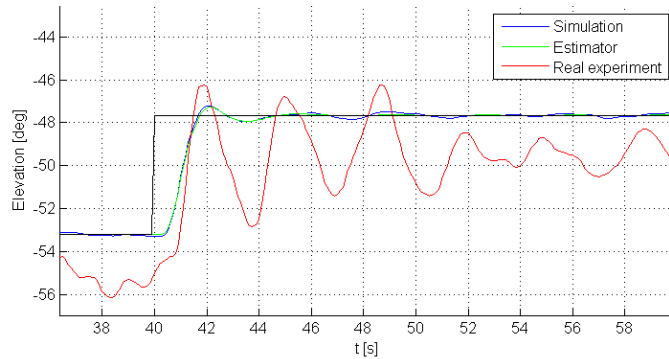
5.2 Discrete Linear Quadratic Regulator (DLQR) simulation



dlqr/carousel_dynamics()

5.3 DLQR experimental results

First attempt



5.4 Disturbance state augmented DLQR design

- Linearization at $x_{ss} = [1.6196 \quad -0.8802 \quad -0.0696 \quad 0 \quad 0 \quad 0 \quad 1.6196]$
- Discretization with $\Delta_t = 20ms$

$$x = \begin{bmatrix} \dot{\delta}_{arm} \\ \ddot{\delta}_{arm} \\ \alpha \\ \beta \\ \dot{\alpha} \\ \dot{\beta} \\ \dot{\delta}_{motor_sp} \\ S_p \end{bmatrix}$$

$$Q = \begin{bmatrix} q_0^2 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & q_0^2 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 10^2 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 7^2 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 5^2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 3^2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & q_0 \end{bmatrix}$$

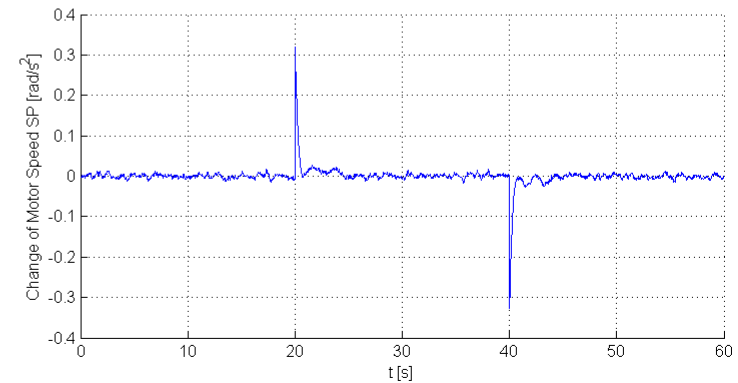
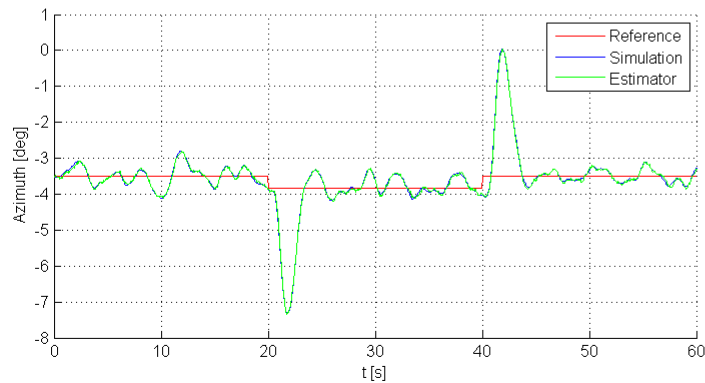
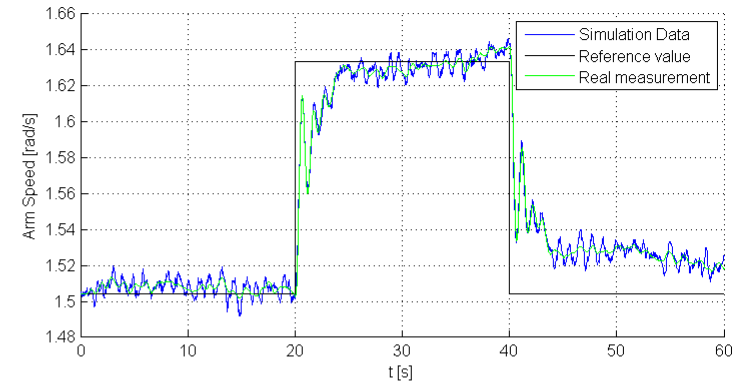
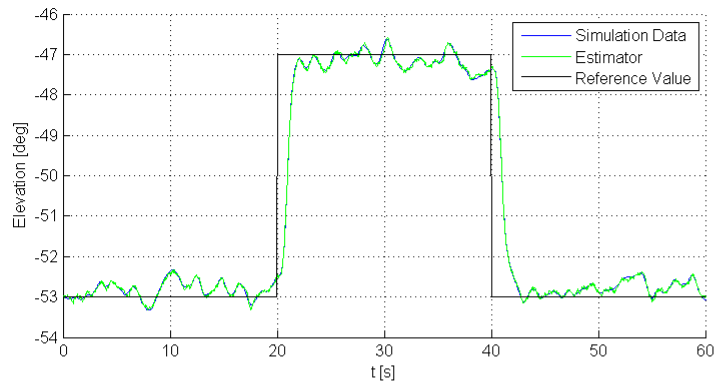
$$q_0 = 1 \times 10^{-6}$$

$$R = [5^2]$$

$$P_N = [0]$$

5.5 Disturbance state augmented DLQR simulation

***Experimental results to be seen during the visit**



Thanks for your attention