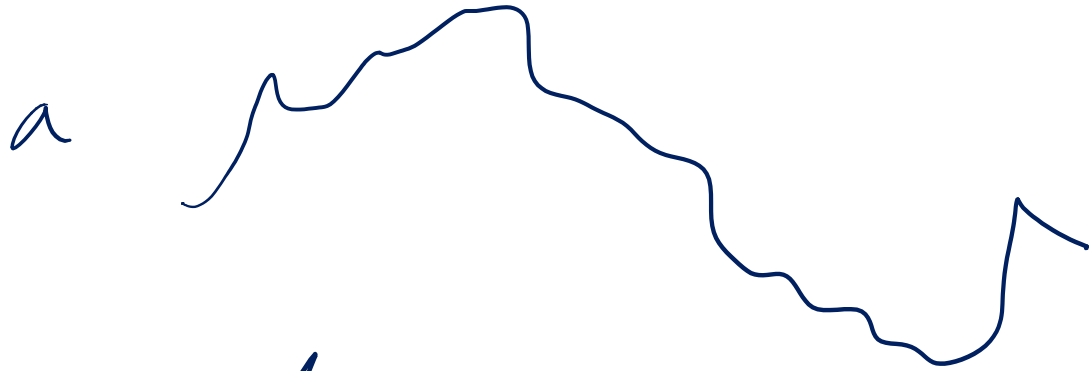


REHEARSAL LECTURE

$$\dot{a} = w$$



CH 8 & CH 9

CH 8 FREE DOM. ESTIMATION

LTI - CONT. SYSTEMS

$$\dot{Y} = U - Y$$

TIME DOM

0



$$sY = U - Y$$

LAPL. DOMAIN

$$(s+1)Y = U$$

$$\frac{Y}{U} = \frac{1}{s+1}$$

$$G(s) = \frac{Y(s)}{U(s)} = \frac{1}{s+1}$$

$G(j\omega)$ GIVES BODE DIAGRAM

DISCRETE TIME SIGNALS & FOURIER TRANSFORM

NYQUIST FREQUENCY ?

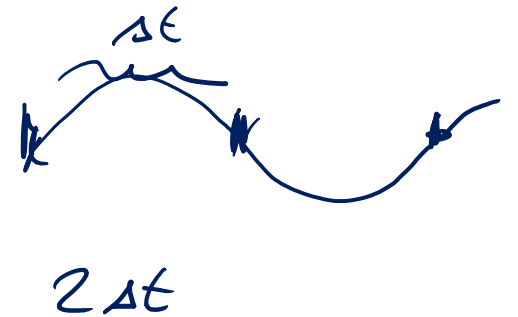
$$f_{Ny} = \frac{1}{2\Delta t}$$

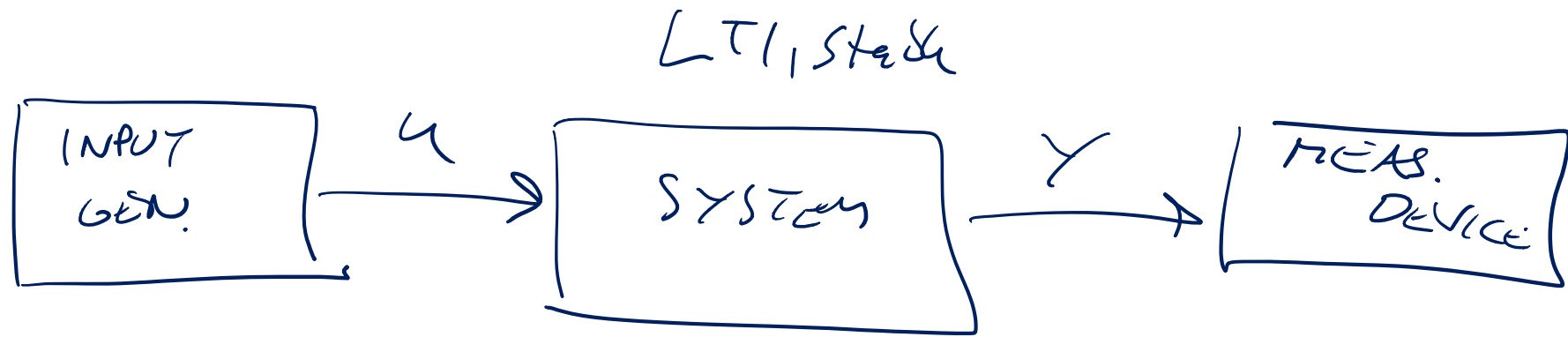
$$\omega_{Ny} = 2\pi \cdot f_{Ny} = \frac{\pi}{\Delta t}$$

IN PRACTICE, SAMPLE ONLY SIGNALS UP TO HALF NYQUIST

IF WE ARE CLOSE OR ABOVE NYQUIST, AN ERROR OCCURS:

ALIASING

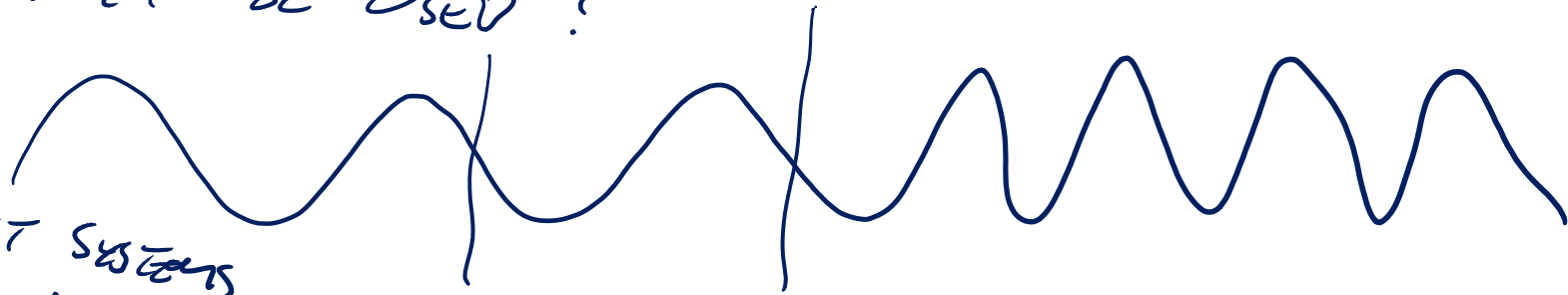




WHAT INPUT SIGNALS MIGHT BE USED?

1. FREQUENCY SWEEP

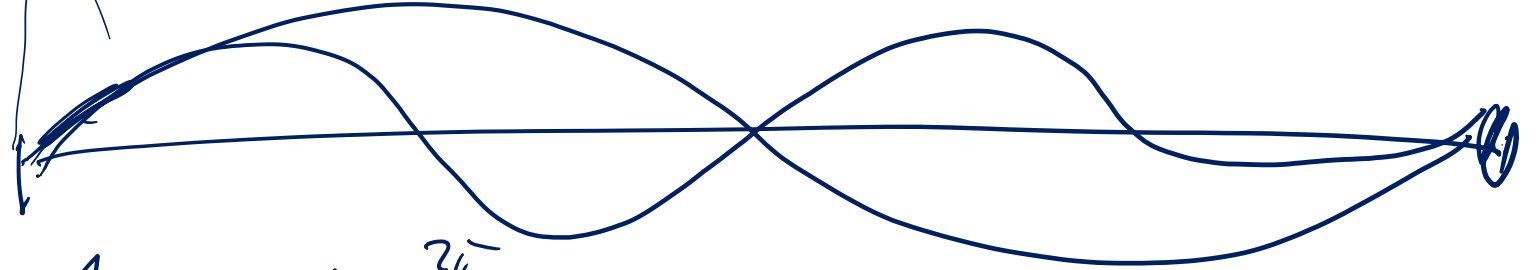
GOOD FOR VERY FAST SYSTEMS
(kHz - MHz range)



2. MULTISINE EXCITATION

WINDOW LENGTH T

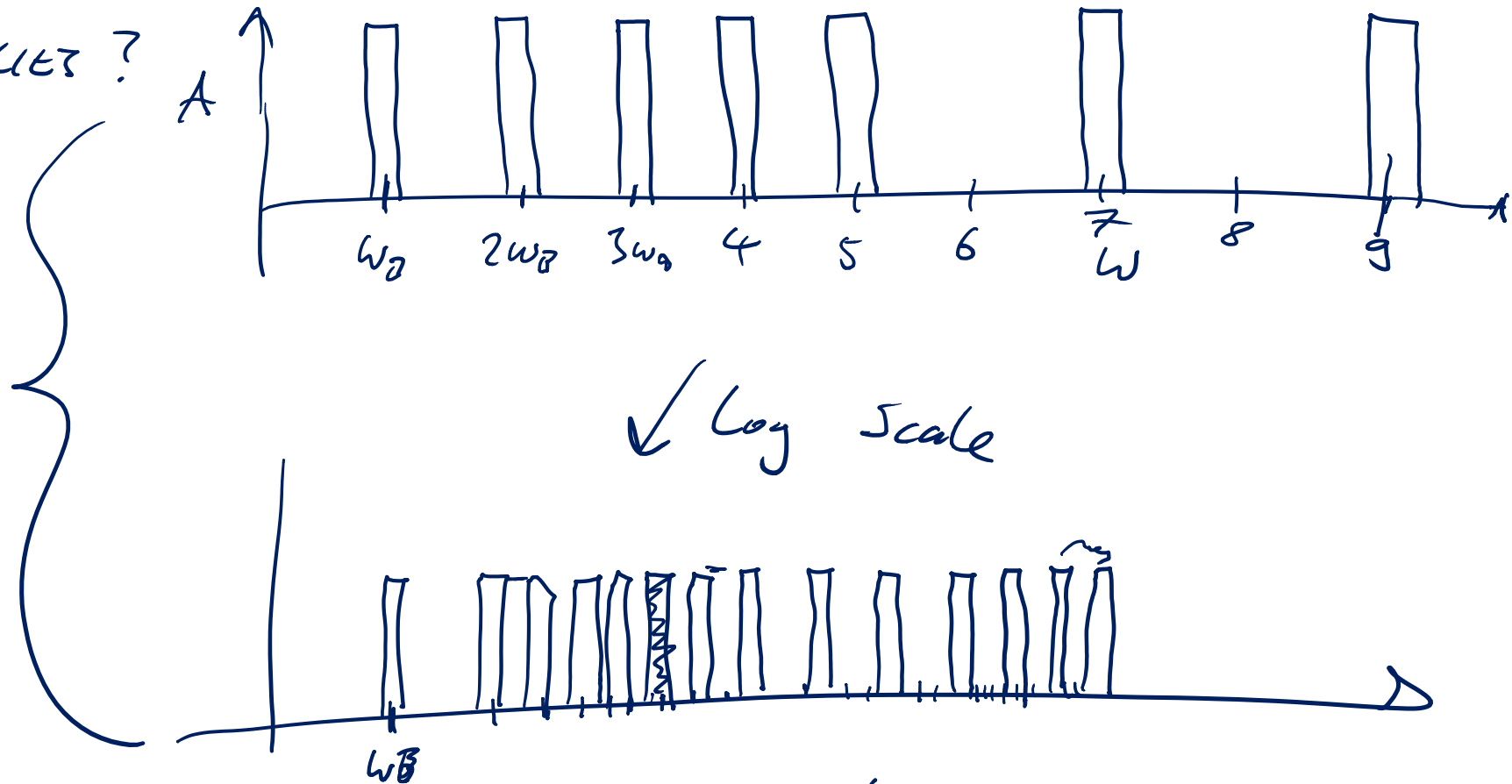
BASE FREQUENCY: $f_B = \frac{1}{T}$, $\omega_B = \frac{2\pi}{T}$
& MULTIPLES



$T = N \cdot \Delta t$
(to avoid "LEAKAGE" errors)

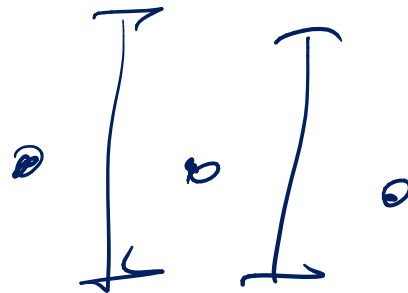
WHICH FREQUENCIES?

AMPLITUDE



PHASE?

- NOT ALIGNED
- RANDOM
- SCHRÖDER PHASES
- OPTIMIZED FOR CREST FACTOR



$$\frac{\omega_{k+1}}{\omega_k} \approx 1.05$$

BUT $\omega_k = \omega_0 \cdot \prod_{i=1}^k p(i)$

↑
INTEGER.

CREST FACTOR

$$CF = \frac{\max}{RMS} = \frac{\max_{t \in [0, T]} |u(t)|}{\frac{1}{T} \int_0^T |u(t)|^2 dt}$$

$$\left(= \frac{\max |u(t)|}{\text{ROOT (AVERAGE ~~PO~~ AMPLITUDE$$

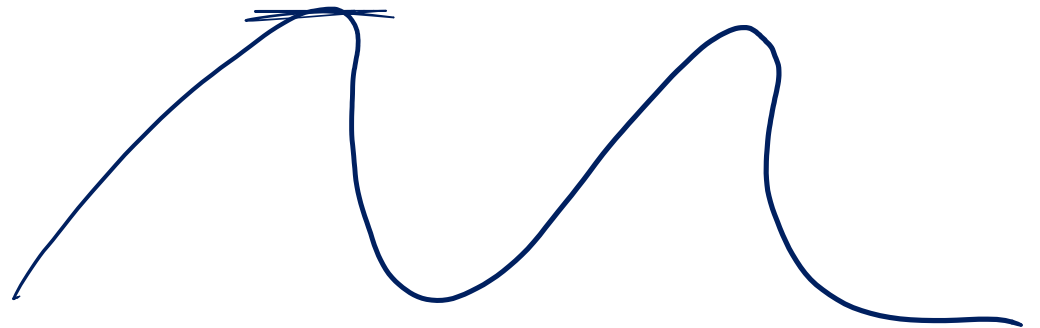
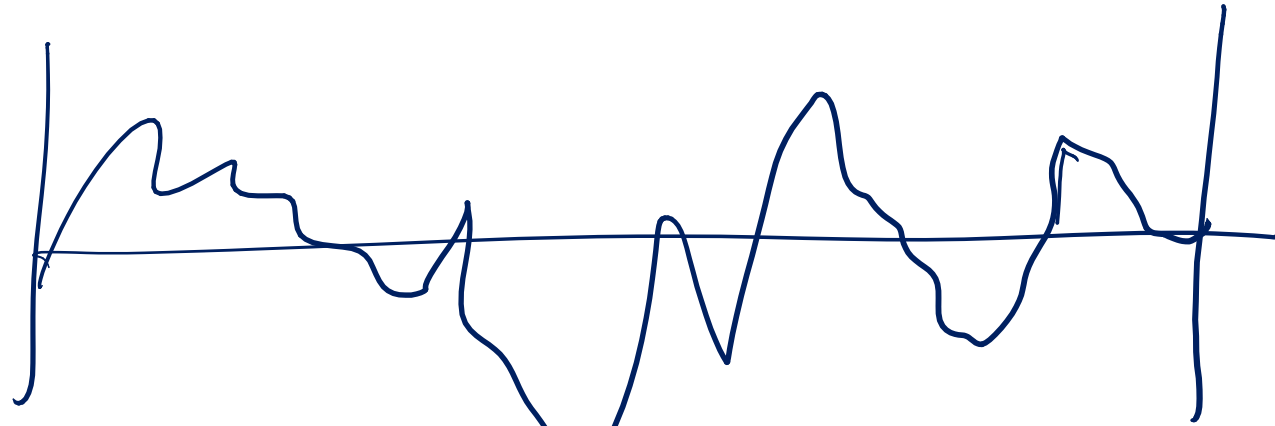
ON FREQUENCY
DOMAIN)

RA PARSEVAL'S THEOREM

$$u(t) = \sum_{n=1}^N A \cdot \sin(\omega_n \cdot kt + \varphi)$$

$$\int_0^T |u(t)|^2 dt = \sum A^2 \cdot \int_0^T \sin^2(\omega_n k) dt$$

(DUE TO ORTHOGONALITY OF
BASIS FUNCTIONS)



DISCRETE TIME FOURIER

$$\begin{bmatrix} u(0) \\ \vdots \\ u(N-1) \end{bmatrix} \xrightarrow{\quad} \begin{bmatrix} \bar{U}(0) \\ \vdots \\ \bar{U}(N-1) \end{bmatrix} = \begin{bmatrix} \text{"DFT"} \\ \text{MATRIX"} \end{bmatrix} \cdot \begin{bmatrix} u(0) \\ \vdots \\ u(N-1) \end{bmatrix}$$

$$\bar{U} = \overset{\text{ORTHOGONAL}}{M} \cdot \bar{u}$$

$$\bar{U}^T \cdot \bar{U} = \bar{u}^T \underbrace{(M^T M)}_{\text{(DIAGONAL)}} \bar{u} = \sum u(n)^2$$

$$\bar{U} = \underline{\underline{\text{fft}(\bar{u})}}$$

$$\bar{u} = \text{ifft}(\bar{U})$$

$$\bar{u} = \text{ifft}(\text{fft}(u))$$

$$M = \begin{bmatrix} \alpha^0 & \alpha^1 & \alpha^2 & \alpha^3 & \dots \\ \alpha^0 & \alpha^2 & \alpha^4 & \alpha^6 & \dots \end{bmatrix}$$

(OR SIMILAR)

FOURIER MATRIX

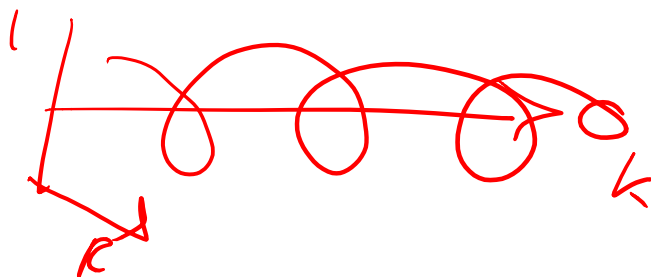
$$= \boxed{M \cdot \bar{u}}$$

$$= \frac{1}{N} M^H \cdot \bar{U}$$

$$= \frac{1}{N} M^H \cdot (M \cdot \bar{u}) = \bar{u}$$

$$= \begin{bmatrix} \text{---} \\ \text{---} \\ \text{---} \\ \text{---} \end{bmatrix}^T$$

$$\alpha = e^{-\frac{2\pi j}{N}}$$



$$M \in \mathbb{C}^{N \times N}$$

$$M^H M = I \cdot N$$

COMPUTED BY
"FAST FOURIER TRANSFORM (FFT)"

AFTER RECORDING THE MULTISINE OUTPUT SIGNAL,
DISCARDING FIRST PERIODS (TRANS.)

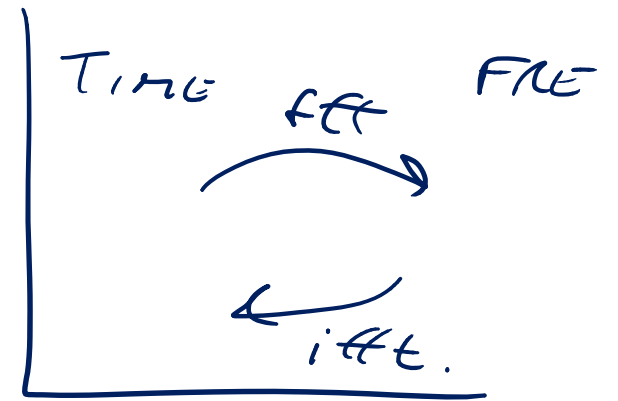
AVERAGING "GOOD" PERIODS

GET ~~$\hat{y}(k)$~~ AND ~~$\hat{u}(k)$~~ ~~$\hat{y}(t)$~~

~~$\hat{y}(k)$~~ FROM ~~IFFT~~ OF ~~$\hat{y}$~~

$$G(j\omega_B \cdot k) = \frac{\hat{y}(k)}{\hat{u}(k)}$$

FOR k IN INPUT SIGNAL



61

sig 6

OUTPUT ERROR VS EQUATION ERROR

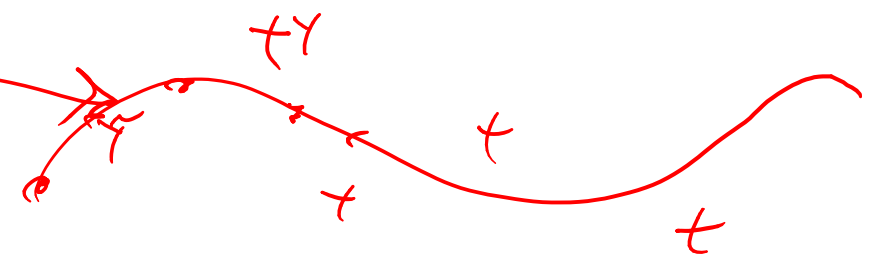
PURE OUTPUT
EQ. ERRORS



$$y(k) = \sum_{i=1}^n a_i y(k-i) + b_i u(k-i) + \varepsilon(k)$$

$\underbrace{\hspace{10em}}_{\text{Pred}}$

TRUE VALUE
&
MEASUREMENT



$$\tilde{y}(k) = \underbrace{\sum a_i \tilde{y}(k-i)}_{\text{Pred}} + u(k)$$

$$y(k) = \tilde{y}(k) + \varepsilon(k)$$