

Exercises 14: Course revision and exam preparation
(Thursday 11.02.2016 at 15:00 in Room SR 00 014)

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1. Consider a process plant that is described by the nominal transfer function

$$\hat{G}(s) = \frac{(3-s)}{(s+1)(s+5)}.$$

with a multiplicative model uncertainty that has as an upper bound

$$\bar{\Delta}_M(s) = 0.1 \cdot \frac{s+1}{\frac{s}{100} + 1}.$$

We want to design a robust and stable discrete-time controller $K_z(z)$ with internal model control (IMC). The goal is to achieve the maximal possible bandwidth for the closed-loop system, while still guaranteeing robust stability. The controller design is done in the continuous-time domain. Afterwards the controller is digitized.

- (a) Is the nominal plant model $\hat{G}(s)$ minimum-phase?
 - (b) Determine the ideal IMC-controller $K_{\text{IMC}}^*(s)$ that minimizes the integral square error (ISE) for step reference inputs. Factorize $\hat{G}(s)$ if necessary.
 - (c) We now add a filter $V_f(s) = \frac{1}{(Ts+1)^n}$ in order to make the controller $K_{\text{IMC}}(s)$ proper. Choose a filter of the lowest possible order to achieve this. Determine a lower limit for the filter time constant T , by taking into consideration the condition for robust stability.
Hint: Draw the Bode-diagram of the robustness limit, computed with the upper bound of the multiplicative uncertainty $\bar{\Delta}_M(s)$.
 - (d) Determine the transfer function of the overall controller $K(s)$.
 - (e) Determine the discrete equivalent $K_z(z)$ of the overall controller $K(s)$ designed above. Use the zero-pole matching method. Use the sampling period $T_p = 25\text{ms}$
2. Consider a process plant described by the transfer function

$$G(s) = \frac{e^{-T_d s}}{(5s+1)(2s+1)}.$$

Design a Smith Predictor that realizes a feedback loop with a settling time $T_s \leq T_d + 3$ sec, and with an overshoot $M_p \leq 10\%$. The dead time $T_d = 42$ sec.

- (a) Design a lead compensator $K_R(s) = k_D \frac{T_D s + 1}{T_D s + 1}$ for the rational part $G_R(s)$ of the process plant, using the root locus method.
 - i. What are the desired pole locations of the closed-loop system poles?
 - ii. Determine the lead zero $\frac{1}{T_D}$ in order to cancel the slowest process pole.
 - iii. Determine the lead pole $\frac{1}{T_D}$ in order to fix the real part of the closed-loop poles.
 - iv. Determine the gain k_D in order to place the closed-loop poles in their desired locations.
 - (b) Compute the resulting closed-loop transfer function $G_r(s)$. Assume that the model of the plant is perfect.
 - (c) What is the steady state error of the closed-loop system for a step input? And for a ramp input?
 - (d) Design a prefilter feedforward controller $K_{\text{ff,p}}(s)$ for a servo application, that minimizes the ISE for step reference inputs. The prefilter should reduce the steady state error for a ramp input to $e_{\text{ss}} \leq 0.1$. Check if the dynamic requirements are still met.
3. A process plant $G(s)$ can be divided into two partial processes $G_1(s)$ and $G_2(s)$ in series. The transfer functions of these partial processes are given by

$$G_1(s) = \frac{3}{(2s+1)(4s+1)} \quad \text{and} \quad G_2(s) = \frac{4}{15s+1}.$$

Design a cascaded controller that realizes a closed-loop system with a bandwidth $\omega_{\text{BW,cl}} \approx 0.04 \frac{\text{rad}}{\text{s}}$.

- (a) Design a causal controller $K_1(s)$ with internal model control (IMC) for the inner loop process $G_1(s)$. Minimize the Integral Square Error (ISE). Make sure that the inner loop bandwidth is approximately $\omega_{\text{BW,1}} \approx 0.25 \frac{\text{rad}}{\text{s}}$.

- (b) Approximate the obtained inner closed-loop system by a first order system $G_a(s) = \frac{k_a}{T_a s + 1}$.
- (c) Design a realizable controller $K_2(s)$ with internal model control (and with minimal ISE) for the overall process $G_a(s)G_2(s)$. Make sure that the bandwidth requirement is met.
- (d) Evaluate the validity of the approximation of the inner closed-loop system, computed in 3b.

4. Consider the following system, of which the state space model is decomposed into Kalman form:

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 2 & -3 & 0 \\ 0 & -1 & 0 \\ 2.8 & 0 & -2 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} \sqrt{2} \\ 0 \\ -2 \end{bmatrix} u(t)$$

$$y(t) = \begin{bmatrix} \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & 0 \end{bmatrix} \mathbf{x}(t).$$

- (a) Evaluate the controllability and observability of the different states.
- (b) Is the system controllable? If not, is it stabilizable? Is the system observable? (If not, is it detectable?)
- (c) Compute the transfer function of this system. Also, determine that state space model that is a minimal realization of this transfer function.
- (d) Given the state space model obtained in 4c, determine the desired pole locations $\lambda_{cl,i}$, so that the closed-loop system has a settling time $T_s \leq 0.3$ sec.
- (e) If the system is *at least* stabilizable and detectable, determine by ‘comparison of coefficients’ the feedback controller matrix \mathbf{K} that places the closed-loop poles at the desired locations $\lambda_{cl,i}$.

Peak time T_m	$\frac{\pi}{\omega_0 \sqrt{1-\zeta^2}}$	ϕ_ζ	ζ	Δh
Rise time T_r	$\frac{1.8}{\omega_0}$	66°	0.4	25%
Settling time $T_{5\%}$	$\frac{3}{\zeta \omega_0}$	54°	0.58	10%
Settling time $T_{2\%}$	$\frac{4.5}{\zeta \omega_0}$	45°	0.7	5%
		37°	0.8	2%

Table 1: Dynamic behaviour heuristics of a second order system with complex conjugate poles $\zeta \omega_0 \pm j \omega_0 \sqrt{1 - \zeta^2}$.

Rise time T_r	$\frac{2.2}{ s_1 }$
Settling time $T_{5\%}$	$\frac{3}{ s_1 }$

Table 2: Dynamic behaviour heuristics of a first order system.

Rise time T_r	$\frac{3.36}{ s_{1/2} }$
Settling time $T_{5\%}$	$\frac{4.8}{ s_{1/2} }$

Table 3: Dynamic behaviour heuristics of a second order system with a double negative real pole.